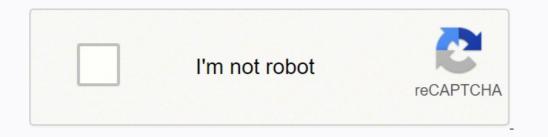
<u>3 phase motor current calculator kw</u>

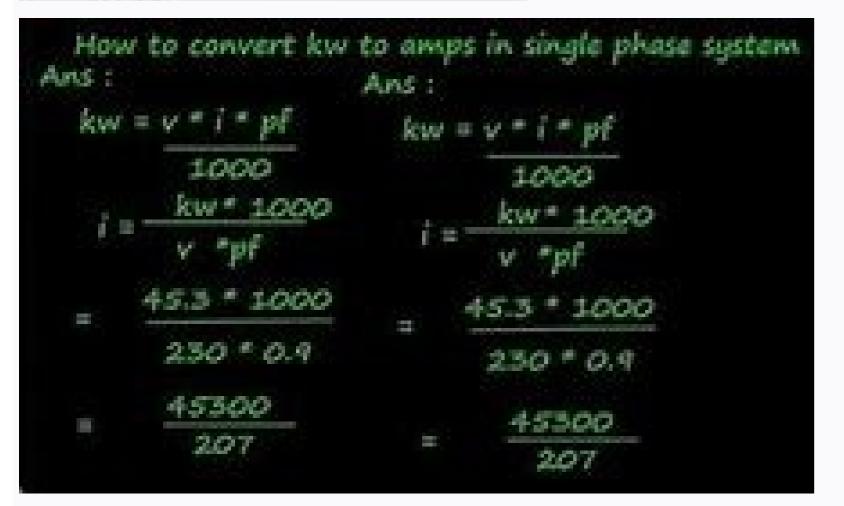




3 phase motor current calculator kw

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Three Phase Load

Calculating kVA and kW (Three Phase)

Formula: $kVA = V \times I \times \sqrt{3} \div 1000$ Where: V = Volts generatedI = Amps availableP.F. - Power factor of load (Usually 0.8) $\sqrt{3} = 1.732$

Example 1

A 415 volt, three phase generator provides 200 Amp. Calculate t kW and kVA of this generator. kW = V x1 x P.F. x $\sqrt{3}$ + 1000 = 415 x 200 x 0.8 x 1.732 + 1000 = 115 kW

 $kVA = kW \div P.F. = 115 \div 0.8 = 143 kVA$

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One can ask: $\hat{a} \in \hat{c}$ What is exactly a constant? "An example of a constant with which he is very familiar is PI ($\hat{a} \in$), which is derived by dividing the circumference and the respective circle diameter, your relationship is always pi. You can use constants that apply to specific single-phase and three-phase voltages to calculate the current (I) and the kilowatts (KW). Let's see how it is done. Monopassic CALLS Bassical theory Theory tells us that for a monophastic system, $kW = (v \tilde{A} \notin \tilde{A} \tilde{A} \tilde{a} \notin (1,000)$. For the sake of simplicity, we assume that the power factor (PF) is unity. Therefore, the previous equation becomes $KW = (V \tilde{A} \hat{a} \hat{a} + (1,000)$. For the sake of simplicity, we assume that the power factor (PF) is unity. 1,000. Resolving for I, the equation becomes $i = 1,000 \text{kw} \cdot V$ (equation 1) now, if you look at the part of «1,000 $\cdot \hat{a} \in \hat{a} \in \hat{c}^2$ of this equation, You can see that by inserting the respective single-phase voltage for «VÃ $\notin \hat{a} \in \hat{c}^2 \hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{c}^2 \hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{c}^2$ and divide it into« 1000 $\hat{a} \in \hat{c}^2$ and divide it into» (or constant) number that is You can use to multiply $\hat{A} \in KW$ » to obtain the current of that load on the respective voltage. For example, the constant for the calculation of 120V is 8.33 (1,000 · 120). Using this constant, equation 1 becomes I = 8.33kw. Therefore, if you have a load of 10kw, you can calculate the current thrust at 83.3a (10 to 8.33). If you have a computer that extracts 80a, then you can calculate the relative size of the required energy source, which is 10kw (80 to 8.33). Table 1. Constants used in single-phase systems using this same procedure but introducing the respective monophastic voltage, the following monofessional constants are obtained, as shown in Table 1. Trifics for TRIFA systems Sicos, we use the following equation: kW = (V ÅfÅ- Å Å å € Åfå- 1,732) ÅfÅ · 1,000. Once again, assuming the PF unit and solving this equation for Å «IÅ», you get: I = 1,000kw A Table 2. Constants used in three-phase voltage for "V" and multiplying it by 1,732, you can divide that amount into "1,000" to get a specific (or constant) number that you can use to multiply "kW" to get the current of that three-phase load at the respective three-phase voltage. Table 2 lists each three-phase voltage obtained from the previous cycle. The Start and Running Current Calculator from getcalc.com is an online electrical engineering tool for calculating the starting current, operation and full load of a three-phase AC induction motor. Starter current, sometimes abbreviated as Istart in electrical engineering, is a measurement or classification of the AC induction motor. the amount of current required for a one- or three-phase AC motor to start. Usually four times current. Similarly, Current On, sometimes abbreviated as Irun, is the current required for an AC induction motor to operate freely without charge after starting. Similarly, Full-loadent, sometimes abbreviated as Ifull-load, is the current required for an AC induction motor to operate at its maximum load or rated power. The unit of current medicine is Amps often used as amps. Formulas for calculate the full load current of AC induction motors with this free online motor current calculator. Includes Formulas. Tension (V). The phase-to-phase voltage for a three-phase power supply, or the phase-to-neutral voltage for a single-phase power supply. Phase. Either a three-phase or single-phase voltage source. Qualification (P). Engine power value in kW or CV. Power factor (like that). The rated engine power factor. Typically around 0.86. Efficiency (·). The efficiency of the engine. Typically around 95%. Enter 95. \ (i = \ DisplayStyle \ Frac {1000 \ cdot v_ {ll} \ cdot \ cos {\ PHI} \ cdo phase with kilovatios power (KW): \ (i = \ displayStyle \ Frac {1000 \ CDOT P_ {KW}} {V_ {LN} \ cos {\ PHI } \ cdot \ eta}) Note that the nominal full load current of the motor is specified in the motor sheet and SE Stamp on the engine name plate. However, this calculator is useful when only the power of the motor is available and an estimate of the current is required. The chemulas and calculations contained below should only be used for estimation purposes. It is the responsibility of the client to specify the HP engine, the torque and the acceleration time needed for its application. The seller may want to check the values specified by the client must hire a Electric engineer to perform the exact calculations. For a detailed explanation of each chemula, click on the links below to go directly to it. Pair in lb.ft. = HP x 5250RPM ----- HP = torque x rpm ----- rpm = 120 x Firm frequency. of poles5250 temperature conversionmule = 1.8 k + 0.6ão .k = 5/9 (Ã , or-0.6ão) AOF = 1.8 Å, OC + 32 Å, OC = 5/9 (Å, of-32ão) jÃ.or = AOF + 460ÅO, K = A.OC + 273Å, OC = celsius, degrees Å, k = Kelvin Å, or = Rankine, Degrees Å, k = Kelvin Å, or = Rankine, Degrees Å, k = Kelvin Å, or = Rankine, Degrees Å, A and the temperature A aoF 371.1398.9426.7454.4482.2 700 750 800 850 900 1292.01 382.01 472.01 562.01 652.0510.0537.8565.6593.3621.1 9 501 000 105 011 001 150 150 648.9676.7704.4732.2 1 200 125 013 001 350 2192.02 282.02 372.02 462.0 to Oc Oc Temperature at 760.0787.8815.6843.3872.1 14 001 450 150 015 501 600 2552.02 642.02 732.02 822.02 912.0899.9927.7955.4983.21 011.0 16 501 700 175 018 001 850 3002.03 092.03 182.03 272.03 362.0 1038.81 066.61 094.31 121.1 1 900 195 020 002 050 3452.03 542.03 632.03 722.0 T = WK2 X RPM308 x T AV .---- WK 2 = inertia in lb.ft.2t = acceleration time in sec.t = Av. Speeling torque lb.ft.t = WK2 x RPM308 X tinercia reflected to the motor = load inertia load rpmmotor rpm 2ns = 120 x fp ----- f = p x ns120 ----- f = p x ns120 ----- p = 120 x fnshp = t x n5250 ----- t = 5250 HPN ----- N = 5250 HPN ----- N = 5250 HPT & Sliding = NS â & "NNSX 100Codekva / HPÃ, Codekva / -7.09Å, N11.2-12.49Å, U20.0-22.39D4.0 -4.49Å, 17.1 -7.99Å, P12.5-13.99Å, V22.4 & UPE4 .5 -4.99Å, R14.0-15. I = current in amperose = voltioskw tension = Kilovatioskva power = apparent power in kilovolts-amperioshp = output power in force horses = motor speed in revolutions per minute (RPM) NS = Sindish speed in revolutions per din revolutions per minute (RPM) NS = Sindish speed in revolutions per din revolutions per minute (RPM) NS = Sindish speed in revolutions per din revolutions per din revolutions per minute (RPM) NS = Sindish speed in revolutions per din minute (RPM) P = PoloSF number = Frequency in cycles per second (CPS) T = torque in pounds-pitch = efficiency as decimalpf = power factor such as decimalpf = power f main motor. The total WK2 equivalent for a system is the sum of the WK2 of each piece, referenced at the speed of the main motor. Equation is converted into a common denominator in which other catners can be based. In the case of variable speed devices, the inertia must be calculated first at low speed. Let's see a simple system that a main engine (PM), a gearbox and a load. WK2 = 100 lb.ft.2Ã" WK2 = 900 lb.ft.2 (as seen on the output axis)" WK2 = 27,000 lb.ft.2The formula indicates that the equivalent system WK2 is equal to the of WK2parts in the RPM of the main engine, or in this case: Ã WK2EQ = WK2pm + WK2Red. Red. RPMPM RPM 2+ WK2Load Load RPMPM RPM 2Note: reducer RPM = Load RPM = WK2EQ = WK2pm + WK2Red. 13 2+ WK2Load 13 2The WK2 of the main engine plus the WK2 of the main engine, plus the WK2 of the gearbox times (1/3) 2, plus the WK2 of the load times (1/3) 2, plus the WK2 of the load times (1/3) 2. This ratio of the reducer to the driven load is expressed by the formula given above: A" WK2EQ = WK2part NpartFirst engine 2In other words, when a part rotates at a speed (N) different from that of the main engine, the WK2EQ is equal to the WK2EQ is equal to the WK2EQ is equal to the speed ratio of the speed 245 V. = 100 x 254V / 230V IL @ 245V. = 107 AMPERIOS HORSEPOWER is a job done by time unit. An HP is equivalent to 33,000 LB of work per minute. When working with a torque source (T) to produce rotations (M) on an axis, the work done is: A, radio x 2 x rpm x lb. or 2 tmcuando the rotation is at speed n rpm, the HP delivered is: HP = Radio x 2 x rpm x lb.33,000 = TN5,250 for vertical or lifting movement Ã, HP = W x S33,000 x EwaquÃ, W = total weight in pounds. It should be raised by the Motors = lifting speed by Minutoe = general mechanical efficiency of the elevator and gear. To estimate E = .65 for EF. Boat and connected equipment. For fans and blowers: Ã, HP = volume (CFM) x Head (inches of water) 6356 x ventilator mechanical efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. per square foot) 3300 X Mechanical efficiency of the fan Efficiency of the fan Efficiency of the fan Efficiency of the fan Efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency of the fan Efficiency of the fan Efficiency of the fan Efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency of the fan Efficiency of the fan Efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency of the fan Efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency of the fan Efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency \tilde{A} , HP = Volume (CFM) x pressure (LB. by SQ. IN.) 229 X Mechanical efficiency \tilde{A} and \tilde{A} and speed. The developed pressure varies with the square speed square. HP varies with the fan speed cube. For pumps: Ã, HP = gpm x press on LB. By sq. IN. x Specific gravity1713 x Mechanical efficiency of Bombo Ã, HP = GPM x Total dynamic head in feet x Specific gravity3960 x Mechanical pump efficiency, where total dynamic head = Static head + friction head Estimation, the efficiency of the pump can be assumed by 0.70. Accelerate the system running. However, start or accelerate the system requires additional energy. The pair required to accelerate the system running. However, start or accelerate the system running. change in RPM, divided by 308 times the interval (in seconds) at which this acceleration occurs: N=Change in RPMW=Weight in lbs.K=Girotation radius=T time of (secs.) WK2=Equivalent Inertia308=Proportionality ConstantO TAcc acceleration due to gravity. If, for example, we simply have a main engine and a load without speed adjustment: Example 1 WK2 = 200 lb.ft.2 WK2 = 800 lb.ft information to find the amount of torque needed to accelerate the charge. The formula says: A TAcc = WK2EQN308tor 1000 x 1 800 308 x 600 180 480In other words, 97.4 lb.ft. of torque must be applied to get this load to turn at 1800 RPM, in 60 seconds. Note that TAcc is an average value of the acceleration torque during the speed change considered. If you want a more accurate calculation, the following example may be useful. Example 2 The time it takes to accelerate an induction engine from the following equation: A" t = WR2 x change in rpm308 x TDonde: A" T=Average value of the acceleration torque during the change of speed considered t=Time it takes the engine to accelerate from initial speed to the final speed. Heel effect, or moment of inertia, for the driven machine must refer to the motor axis). The application of the above formula will be considered below with an example. Figure A shows the speed-torque curves of an induction motor with a squirrel cage and a driving blower. At any blower speed, the difference between the torque available for acceleration. The reference to Figure A shows that the acceleration torque can vary greatly with speed. When the curves For the engine and blower cross no available pair available Acceleration. Then, the engine drives the blower at constant speed and delivers only the torque required for the load. To determine the total time required to accelerate the engine and the blower, the area between the engine's speed-torque curve and the blower's speed-torque curve is divided into strips whose ends are close to the straight lines. Each band corresponds to a speed increase that takes place within a defined time interval. The solid horizontal lines are the mean acceleration torgues for the selected speed ranges. To calculate the total acceleration time of the engine and the direct coupling blower, it is necessary to find the time needed to accelerate the engine from the start of one speed intervals to arrive at the total acceleration time. If the WR2 of the engine whose speed-torque curve shown in Figure A is 3.26 ft.lb.2 and the WR2 of the blower referring to the engine shaft is 15 ft.lb.2, the total WR2 is: $\tilde{A}^{"}$ 15 + 3.26 = 18.26 ft.lb.2, and the total acceleration time is: $\tilde{A}^{"}$ WR230 8rpm1T1+rpm2T2+rpm3T3+ \hat{a} - \hat{a} + rpm9T9O t = 18.2 630 815 046+15 048+30 047+30 043.8+20 039.8+20 036.4+30 032.8+10 029.6+4011Curves used to determine the time required for the time required for the time required for the time required to determine Accelerate Speed Induction Motor and Accelerate Speed Induction Blower Torques T1 = 46 lb.ft. T3 = 47 lb.ft. T3 = 47 lb.ft. T3 = 47 lb.ft. T4 = 43.8 lb.ft. T7 = 32.8 lb.ft. T5 = 39.8 lb.ft. special characteristics such as: -----Â"Suitable for 10 starts per hourÂ"O----Â"Suitable for 3 setbacks per minuteÂ"Or-----Â"Suitable for 5 starts and stops per hourÂ"Orders with notes like these They are processed for two reasons. First, you must consulted on the corresponding product category to determine if a design is available that: which: perform the required work cycle and, if not, determine whether the type of design required corresponds to our current product line. None of the above notes contains sufficient information should include the following: Reflected inertia on the engine axis. Torque load on the engine during all parts of the working cycle, including starting, operating times, stops or turns. The exact time of each part of the cycle is carried out. For example, a stop can be by means of sailing, mechanical braking, dynamic braking DC or plug. The inversion can be achieved by the plug, or the engine can be stopped by some means and then restarted in the opposite direction. When the engine is running at multiple speeds, the cycle for each speed must be fully defined, including the method of switching from one speed to another. Any special mechanical problems, characteristics or limitations. Getting this information and consulting with the product group before placing the order can save a lot of time, expense and correspondence. The work cycle that is repeated over a given period of time. This cycle may include frequent starts, plug stops, reversals, or stops. These characteristics are normally involved in batch processes and may include drum barrels, certain cranes, shovels and dredgers, shock absorbers, door or plough placement drives, drawbridges, loading and personnel lifts, press type extractors, some feeders, press type kneading machines, pulling cars, (Fundición or Automobile), the cuisine and washing machines, and certain merchandise and passenger transport vehicles. The list is not exhaustive. The drives of these loads should be able to absorb the heat generated during the service cycles. A suitable red capacity would be required in sliding slip Clutches or motors to accelerate or plug these units or to support posts. It is the product of the sliding speed and the torgue absorbed by the load per unit of time that generates heat in these components of the unit. All events that occur during the working cycle generate heat that the components of the unit must dissipate. Due to the complexity of the work cycle cycles and the extensive engineering data by design and qualification of specific motors required for the cycles, it is necessary that the client refer to an electrical engineer for the size of the engine with a work cycle application. Application.

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